Dual 1.5MHz, 600mA Synchronous Step-Down Converter

## Features

- 600 mA Output Current on Each Channel
- 2.5 V to 5.5 V Input Voltage Range
- 1.5 MHz Constant Frequency Operation
- Low Dropout Operation at 100\% Duty Cycle
- Synchronous Topology
- 0.6V Low Reference Voltage
- Typically 0.1 $\mu \mathrm{A}$ Shutdown Current
- Current Mode Operation
- Over-Temperature Protection
- Over-Current Protection
- Up to $94 \%$ Efficiency
- Internally Compensated
- Lead Free and Green Devices Available
(RoHS Compliant)


## Applications

- TV Tuner/Box
- Portable Instrument


## General Description

The APW7134 contains two independent 1.5 MHz constant frequency, current mode, and PWM step-down converters. Each converter integrates a main switch and a synchronous rectifier for high efficiency without an external Schottky diode. The APW7134 is ideal for powering portable equipment that runs from a single cell LithiumIon (Li+) battery. Each converter can supply 600 mA of load current from a 2.5 V to 5.5 V input voltage. The output voltage can be regulated as low as 0.6 V . The APW7134 can also run at $100 \%$ duty cycle for low dropout applications.

## Pin Configuration



## Ordering and Marking I nformation

| APW7134 |  | Assembly Material <br> Handling Code <br> Temperature Range <br> Package Code | Package Code <br> QA : DFN3×3-10 <br> Temperature Range I: -40 to $85^{\circ} \mathrm{C}$ <br> Handling Code <br> TR : Tape \& Reel <br> Assembly Material <br> G: Halogen and Lead Free Device |
| :---: | :---: | :---: | :---: |
| APW7134 QA: | APW <br> 7134 <br> XXXXX |  | XXXXX - Date Code |

Note: ANPEC lead-free products contain molding compounds/die attach materials and 100\% matte tin plate termination finish; which are fully compliant with RoHS. ANPEC lead-free products meet or exceed the lead-free requirements of IPC/JEDEC J-STD-020D for MSL classification at lead-free peak reflow temperature. ANPEC defines "Green" to mean lead-free (RoHS compliant) and halogen free ( Br or Cl does not exceed 900ppm by weight in homogeneous material and total of Br and Cl does not exceed 1500 ppm by weight).
ANPEC reserves the right to make changes to improve reliability or manufacturability without notice, and advise customers to obtain the latest version of relevant information to verify before placing orders.

Absolute Maximum Ratings (Note 1)

| Symbol | Parameter | Rating | Unit |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN1/N2 }}$ | Input Supply Voltage (IN1/IN2 to GND1/GND2) | -0.3 ~ 6 | V |
| $\mathrm{V}_{\text {FB1/FB2 }}$ | Voltage on FB1 and FB2 | $-0.3 \sim \mathrm{~V}_{\mathrm{IN1/1N2}}+0.3$ | V |
| $\mathrm{V}_{\text {EN1/EN2 }}$ | Voltage on EN1 and EN2 | $-0.3 \sim \mathrm{~V}_{\mathrm{IN} 1 / \mathrm{N} 2}+0.3$ | V |
| $\mathrm{V}_{\text {SW1/SW2 }}$ | Voltage on SW1 and SW2 | $-0.3 \sim \mathrm{~V}_{\mathrm{IN} 1 / \mathrm{N} 2+0.3}$ | V |
| ISW_PEAK | Peak SW Current | 1.3 | A |
| $\mathrm{T}_{J}$ | Junction Temperature | 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {STG }}$ | Storage Temperature | -65 ~ 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {SDR }}$ | Maximum Lead Soldering temperature, 10 Seconds | 260 | ${ }^{\circ} \mathrm{C}$ |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## Thermal Characteristics

| Symbol | Parameter | Typical Value | Unit |
| :---: | :---: | :---: | :---: |
| $\theta_{\mathrm{JA}}$ | Junction-to-Ambient Resistance in Free Air ${ }^{\text {(Note 2) }}$ | 50 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

Note 2: $\theta_{\mathrm{JA}}$ is measured with the component mounted on a high effective thermal conductivity test board in free air. The exposed pad of package is soldered directly on the PCB.

Recommended Operating Conditions (Note 3)

| Symbol | Parameter | Range | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {IN1/N2 }}$ | Input Supply Voltage (IN1/IN2 to GND1/GND2) | $2.5 \sim 5.5$ | V |
| R2/R4 | Feedback Resistance | $\sim 200$ | $\mathrm{k} \Omega$ |
| $\mathrm{l}_{\text {Out }}$ | Output Current | $\sim 600$ | mA |
| $\mathrm{~T}_{\mathrm{A}}$ | Operating Ambient Temperature | $-40 \sim 85$ | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{J}$ | Operating Junction Temperature | $-40 \sim 125$ | ${ }^{\circ} \mathrm{C}$ |

Note 3: Please refer to the typical application circuit.

## Electrical Characteristics

The * denotes the specifications that apply over $T_{A}=-40^{\circ} \mathrm{C} \sim 85^{\circ} \mathrm{C}$, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| Symbol | Parameter | Test Conditions |  | APW7134 |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{V}_{\text {IN1/N2 }}$ | Each Converter Input Voltage Range |  | * | 2.5 | - | 5.5 | V |
| $\mathrm{l}_{\text {FB1/FB2 }}$ | Each Converter Feedback Current | $\mathrm{V}_{\text {FB1/FB2 }}=0.6 \mathrm{~V}$ | * | -30 | - | 30 | nA |
| $\mathrm{V}_{\text {FB1/FB2 }}$ | Each Converter Regulated Feedback Voltage |  | * | 0.588 | 0.6 | 0.612 | V |
| $\Delta \mathrm{V}_{\text {FB1/FB2 }}$ | Each Converter Reference Voltage Line Regulation | $\mathrm{V}_{\text {(N1/1N2 } 2}=2.5 \mathrm{~V}$ to 5.5 V | * | - | 0.04 | 0.4 | \%/V |
| $\mathrm{l}_{\text {PK }}$ | Each Converter Peak Inductor Current | $\mathrm{V}_{\mathbb{1 N / / \mathbb { N } 2} 2}=3 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=0.5 \mathrm{~V}$ or $V_{\text {out }}=90 \%$, Duty cycle < $35 \%$ |  | 0.75 | 1 | 1.25 | A |

## Electrical Characteristics (Cont.)

The * denotes the specifications that apply over $T_{A}=-40^{\circ} \mathrm{C} \sim 85^{\circ} \mathrm{C}$, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| Symbol | Parameter | Test Conditions |  | APW7134 |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. |  |
| $\mathrm{V}_{\text {LOADR }}$ | Each Converter Load Regulation |  |  | - | 0.5 | - | \% |
| $l_{0}$ | Each Converter Quiescent Current | Duty Cycle $=0 ; \mathrm{V}_{\mathrm{FB}}=1.5 \mathrm{~V}$ |  | - | 300 | 400 | $\mu \mathrm{A}$ |
| $\mathrm{l}_{\mathrm{Q} . \mathrm{SD}}$ | Each Converter Quiescent Current in Shutdown | $\mathrm{V}_{\text {EN1/EN } 2}=0 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=4.2 \mathrm{~V}$ |  | - | 0.1 | 1 | $\mu \mathrm{A}$ |
| fosc | Each Converter Oscillator Frequency | $\mathrm{V}_{\mathrm{FB}}=0.6 \mathrm{~V}$ |  | 1.2 | 1.5 | 1.8 | MHz |
| fosc_FFB | Each Converter Frequency Foldback | $\mathrm{V}_{\mathrm{FB}}=0 \mathrm{~V}$ |  | - | 210 | - | kHz |
| $\mathrm{R}_{\text {DS-P }}$ | Each Converter On Resistance of PMOSFET | $\mathrm{I}_{\mathrm{sw}}=100 \mathrm{~mA}$ |  | - | 0.4 | 0.5 | $\Omega$ |
| R ${ }_{\text {DS }-N}$ | Each Converter On Resistance of NMOSFET | $\mathrm{I}_{\text {sw }}=-100 \mathrm{~mA}$ |  | - | 0.35 | 0.45 | $\Omega$ |
| ILsw | Each Converter SW Leakage Current | $\begin{aligned} & \mathrm{V}_{\text {ENN }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{SW}}=0 \mathrm{~V} \text { or } 5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{IN}}=5 \mathrm{~V} \end{aligned}$ |  | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {EN1EN2 }}$ | Each Converter Enable Threshold |  | * | 0.3 | 1 | 1.5 | V |
| $\mathrm{l}_{\text {EN1/EN2 }}$ | EN1/EN2 Leakage Current |  | * | - | $\pm 0.01$ | $\pm 1$ | $\mu \mathrm{A}$ |

## Typical Operating Characteristics



Oscillator Frequency vs. Supply Voltage





Efficiency vs. Output Current


## Typical Operating Characteristics (Cont.)



## Typical Operating Characteristics (Cont.)



NMOSFET Leakage vs. Temperature


## Pin Description

| PIN |  | FUNCTION |
| :---: | :---: | :---: |
| NO. | NAME |  |
| 1 | EN1 | Channel 1 Enable Control Input. Drive EN1 above 1.5 V to turn on the Channel 1. Drive EN1 below 0.3 V to turn it off. In shutdown situation, all functions are disabled to decrease the supply current below $1 \mu \mathrm{~A}$. There is no pull high or pull low ability inside. |
| 2 | FB1 | Channel 1 Feedback Input. Connect FB1 to the center point of the external resistor divider. The feedback voltage is 0.6 V . |
| 3 | IN2 | Channel 2 Supply Input. Bypass to GND with a $4.7 \mu \mathrm{~F}$ or greater ceramic capacitor. |
| 4 | GND2 | Ground 2. Connected the exposed pad to GND2. |
| 5 | SW2 | Channel 2 Power Switch Output. Inductor connection to drains of the internal PMOSFET and NMOSFET switches. |
| 6 | EN2 | Channel 2 Enable Control Input. Drive EN2 above 1.5 V to turn on the Channel 2. Drive EN2 below 0.3 V to turn it off. In shutdown situation, all functions are disabled to decrease the supply current below $1 \mu \mathrm{~A}$. There is no pull high or pull low ability inside. |
| 7 | FB2 | Channel 2 Feedback Input. Connect FB2 to the center point of the external resistor divider. The feedback voltage is 0.6 V . |
| 8 | IN1 | Channel 1 Supply Input. Bypass to GND with a $4.7 \mu \mathrm{~F}$ or greater ceramic capacitor. |
| 9 | GND1 | Ground 1. Connected the exposed pad to GND1. |
| 10 | SW1 | Channel 1 Power Switch Output. Inductor connection to drains of the internal PMOSFET and NMOSFET switches. |

## Typical Application Circuit



## Block Diagram



Diagram Represents 1/2 of the APW7134

## Function Description

## Main Control Loop

The APW7134 has dual independent constant frequency current mode PWM step-down converters. All the main and synchronous switches are internal to reduce the external components. During normal operation, the internal PMOSFET is turned on, however, it is turned off when the inductor current at the input of $\mathrm{I}_{\text {сомP }}$ to reset the RS latch. When the load current increases, it causes a slight to decrease in the feedback voltage, which in turn, it causes the EA's output voltage to increase until the average inductor current matches the new load current. While the internal power PMOSFET is off, the internal power NMOSFET is turned on until the inductor current starts to reverse, as indicated by the current reversal comparator $I_{\text {RCMP }}$, or the beginning of next cycle. When the NMOSFET is turned off by IRCMP, it operates in the discontinuous conduction mode.

## Pulse Skipping Mode Operation

At light load with a relative small inductance, the inductor current may reach zero. The internal power NMOSFET is turned off by the current reversal comparator, $\mathrm{I}_{\text {RCMP }}$, and the switching voltage will ring. This is discontinuous mode operation and normal behavior for the switching regulator. At very light load, the APW7134 will automatically skip some pulses in the pulse skipping mode to maintain the output regulation. The skipping process modulates smoothly depend on the load.

## Short Circuit Protection

In the short circuit situation, the output voltage is almost zero volts. Output current is limited by the $I_{\text {COMP }}$ to prevent the damage of electrical circuit. In the normal operation, the two straight lines of the inductor current ripple have the same height, it means the volts-seconds product is the same. When the short circuit operation occurs, the output voltage down to zero leads to the voltage across the inductor maximum in the on period and the voltage across the inductor minimum in the off period. In order to maintain the volts-seconds balance, the off-time must be extended to prevent the inductor current run away. Frequency decay will extend the switching period to provide more times to the off-period, and then the inductor cur-
rent have to restrict to protect the electrical circuit in the short situation.

## Dropout Operation

An important detail to remember is that on resistance of PMOSFET switch will increase at low input supply voltage. Therefore, the user should calculate the power dissipation when the APW7134 is used at $100 \%$ duty cycle with low input voltage.

## Slope Compensation

Slope compensation provides stability in constant frequency current mode architecture by preventing sub-harmonic oscillations at high duty cycle. It is accomplished internally by adding a compensating ramp to the inductor current signal at duty cycle in excess of $40 \%$. Normally, this results in a reduction of maximum inductor peak current for duty cycles greater than $40 \%$. In the APW7134, the reduction of inductor peak current is recovered by a special skill at high duty ratio. This allows the maximum inductor peak current to maintain a constant level through all duty ratio.

## Application Information

## Inductor Selection

Due to the high switching frequency as 1.5 MHz , the inductor value of the application field of APW7134 is usually from $1 \mu \mathrm{H}$ to $4.7 \mu \mathrm{H}$. The criteria for selecting a suitable inductor depend on the worst current ripple throughout the inductor. The worst current ripple is defined as $40 \%$ of the fully load capability. In the APW7134 applications, the worst value of current ripple is 240 mA , the $40 \%$ of 600 mA . Evaluate $L$ by equation (1):

$$
\begin{equation*}
\mathrm{L}=\frac{\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {OUT }}\right) \cdot \mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }}} \cdot \frac{1}{\Delta \mathrm{I}_{\mathrm{L}} \cdot f_{\mathrm{S}}} \tag{1}
\end{equation*}
$$

where $f_{S}$ is the switching frequency of APW7134 and $\Delta I_{\llcorner }$is the value of the worst current ripple, it can be any value of current ripple that smaller than the worst value you can accept. In order to perform high efficiency, selecting a low DC resistance inductor is a helpful way. Another important parameter is the DC current rating of the inductor. The minimum value of DC current rating is equal to the full load value of 600 mA plus the half of the worst current ripple, 120 mA . Choosing inductors with suitable DC current rating to ensure the inductors' operation in the saturation.

## Input Capacitor Selection

The input capacitor must be able to support the maximum input operating voltage and maximum RMS input current. The Buck converter absorbs current from input in pulses.


Figure 1.
Figure 1 shows a schematic of a Buck structure. The waveforms is shown as Figure 2.


Figure 2.
Observe the waveform of $I\left(\mathrm{C}_{\mathbb{N}}\right)$, the RMS value of $\mathrm{I}\left(\mathrm{C}_{\text {N }}\right)$ is

$$
\begin{equation*}
\mathrm{I}\left(\mathrm{C}_{\text {IN }}\right)=\sqrt{\left[\left(\mathrm{l}_{\text {OUT }}-\mathrm{I}_{\mathrm{N}}\right)^{2} \cdot \sqrt{\mathrm{D}}\right]^{2}+\left(\mathrm{I}_{\mathrm{N}} \cdot \sqrt{1-\mathrm{D}}\right)^{2}} \tag{2}
\end{equation*}
$$

Replace D and $\mathrm{I}_{\mathrm{IN}}$ by following relation:

$$
\begin{align*}
& \mathrm{D}=\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }}}  \tag{3}\\
& \mathrm{I}_{\mathrm{IN}}=\mathrm{D} \cdot \mathrm{I}_{\mathrm{OUT}} \tag{4}
\end{align*}
$$

The RMS value of input capacitor current equal:

$$
\begin{equation*}
\mathrm{I}\left(\mathrm{C}_{\mathrm{IN}}\right)=\mathrm{I}_{\mathrm{OUT}} \cdot \sqrt{\mathrm{D}(1-\mathrm{D})} \tag{5}
\end{equation*}
$$

When $D=0.5$, the RMS current of input capacitor will be maximum value. Use this value to choose the input capacitor with suitable current rating.

## Application Information (Cont.)

## Output Capacitor Selection

The output voltage ripple is a significant parameter to estimate the performance of a convertor. There are two discrete components that affect the output voltage ripple bigger or smaller. It is recommended to use the criterion has mentioned above to choose a suitable inductor. Then, based on this known inductor current ripple condition, the output voltage ripple consists of two portions; one is the product of ESR and inductor current ripple, and the other is the function of the inductor current ripple and the output capacitance. Figure 3 shows the waveforms to explain the part decided by the output capacitance.


Figure 3.

## Output Capacitor Selection

Evaluate the $\Delta \mathrm{V}_{\text {out1 }}$ by the ideal of energy equalization. According to the definition of $Q$,

$$
\begin{equation*}
\mathrm{Q}=\frac{1}{2}\left(\frac{1}{2} \Delta \mathrm{I}_{\mathrm{L}} \cdot \frac{1}{2} \mathrm{~T}_{\mathrm{S}}\right)=\mathrm{C}_{\text {OUT }} \cdot \Delta \mathrm{V}_{\text {OUT } 1} \tag{6}
\end{equation*}
$$

where $T_{S}$ is the inverse of switching frequency and the $\Delta I_{L}$ is the inductor current ripple. Move the $\mathrm{C}_{\text {out }}$ to the left side to estimate the value of $\Delta \mathrm{V}_{\text {out1 }}$ as the following equation:

$$
\begin{equation*}
\Delta \mathrm{V}_{\text {OUT } 1}=\frac{\Delta \mathrm{L}_{\mathrm{L}} \cdot \mathrm{~T}_{\mathrm{S}}}{8 \cdot \mathrm{C}_{\text {OUT }}} \tag{7}
\end{equation*}
$$

As mentioned above, one part of output voltage ripple is the product of the inductor current ripple and ESR of output capacitor. The equation (8) explains the output voltage ripple estimation.

$$
\begin{equation*}
\Delta \mathrm{V}_{\mathrm{OUT}}=\Delta \mathrm{L}_{\mathrm{L}} \cdot\left(E S L+\frac{\mathrm{T}_{\mathrm{S}}}{8 \cdot \mathrm{C}_{\text {OUT }}}\right) \tag{8}
\end{equation*}
$$

## Thermal Consideration

APW7134 is a high efficiency switching converter, it means less power loss transferred into heat. Due to the on resistance difference between internal power PMOSFET and NMOSFET, the power dissipation in the high converting ratio is greater than the low converting ratio. The worst case is the mainly conduction loss dissipate on the internal power PMOSFET in the dropout operation. The power dissipation nearly is defined as below:

$$
\begin{equation*}
\mathrm{P}_{\mathrm{D}}=\left(\mathrm{I}_{\mathrm{OUT}}\right)^{2}\left[\mathrm{R}_{\mathrm{DS} \text { _ONP }} \cdot \mathrm{D}+\mathrm{R}_{\mathrm{DS} \text { _ONN }} \cdot(1-\mathrm{D})\right] \tag{9}
\end{equation*}
$$

APW7134 has internal over-temperature protection. When the junction temperature reaches 150 centigrade, APW7134 will turn off both internal power PMOSFET and NMOSFET. The estimation of the junction temperature, $T_{J}$, defined as below:

$$
\begin{equation*}
\mathrm{T}_{\mathrm{J}}=\mathrm{P}_{\mathrm{D}} \cdot \theta_{\mathrm{JA}} \tag{10}
\end{equation*}
$$

where the $\theta_{\mathrm{JA}}$ is the thermal resistance of the package utilized by APW7134.

## Output Voltage Setting

APW7134 has the adjustable version for output voltage setting by the users. A suggestion of maximum value of $R_{2}$ is $200 k \Omega$ for keeping the minimum current that provides enough noise rejection ability through the resistor divider. The output voltage programmed by the following equation:

$$
\begin{equation*}
\mathrm{V}_{\text {OUT }}=0.6 \cdot\left(1+\frac{R_{1}}{R_{2}}\right) \tag{11}
\end{equation*}
$$


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## Application Information (Cont.)

## Layout Consideration

The high current paths (GND1/GND2, IN1/IN2, and SW1/ SW2) should be placed very close to the device with short, direct, and wide traces. Input capacitors should be placed as close as possible to the respective IN and GND pins. The external feedback resistors should be placed next to the FB pins. Keep the switching nodes SW1/SW2 short and away from the feedback network.

## Package Information

DFN3x3-10


| SYMBD | DFN3x3-10 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | MILLIMETERS |  | INCHES |  |
|  | MIN. | MAX. | MIN. | MAX. |
| A | 0.80 | 1.00 | 0.031 | 0.039 |
| A1 | 0.00 | 0.05 | 0.000 | 0.002 |
| A3 | 0.20 REF |  | 0.008 REF |  |
| b | 0.18 | 0.30 | 0.007 | 0.012 |
| D | 2.90 | 3.10 | 0.114 | 0.122 |
| D2 | 2.20 | 2.70 | 0.087 | 0.106 |
| E | 2.90 | 3.10 | 0.114 | 0.122 |
| E2 | 1.40 | 1.75 | 0.055 | 0.069 |
| e | 0.50 BSC |  | 0.020 BSC |  |
| L | 0.30 | 0.50 | 0.012 | 0.020 |
| K | 0.20 |  | 0.008 |  |

Note : 1. Followed from JEDEC MO-229 VEED-5.

## Carrier Tape \& Reel Dimensions



SECTION A-A


| Application | $\mathbf{A}$ | $\mathbf{H}$ | $\mathbf{T 1}$ | $\mathbf{C}$ | $\mathbf{d}$ | $\mathbf{D}$ | $\mathbf{W}$ | E1 | F |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DFN3x3-10 | $330 \pm 2.00$ | 50 MIN. | $12.4+2.00$ <br> -0.00 | $13.0+0.50$ <br> -0.20 | 1.5 MIN. | 20.2 MIN. | $12.0 \pm 0.30$ | $1.75 \pm 0.10$ | $5.5 \pm 0.05$ |
|  | $\mathbf{P 0}$ | $\mathbf{P 1}$ | $\mathbf{P 2}$ | $\mathbf{D 0}$ | $\mathbf{D 1}$ | $\mathbf{T}$ | $\mathbf{A 0}$ | B0 | K0 |
|  | $4.0 \pm 0.10$ | $8.0 \pm 0.10$ | $2.0 \pm 0.05$ | $1.5+0.10$ <br> -0.00 | 1.5 MIN. | $0.6+0.00$ <br> -0.40 | $3.30 \pm 0.20$ | $3.30 \pm 0.20$ | $1.30 \pm 0.20$ |

(mm)

## Devices Per Unit

| Package Type | Unit | Quantity |
| :---: | :---: | :---: |
| DFN3x3-10 | Tape \& Reel | 3000 |

## Taping Direction Information

DFN3x3-10


## Classification Profile



## Classification Reflow Profiles

| Profile Feature | Sn-Pb Eutectic Assembly | Pb-Free Assembly |
| :---: | :---: | :---: |
| Preheat \& Soak <br> Temperature min ( $\mathrm{T}_{\text {smin }}$ ) <br> Temperature max ( $\mathrm{T}_{\text {smax }}$ ) <br> Time ( $\mathrm{T}_{\text {smin }}$ to $\mathrm{T}_{\text {smax }}$ ) ( $\mathrm{t}_{\mathrm{s}}$ ) | $\begin{gathered} 100{ }^{\circ} \mathrm{C} \\ 150^{\circ} \mathrm{C} \\ 60-120 \text { seconds } \end{gathered}$ | $\begin{gathered} 150^{\circ} \mathrm{C} \\ 200^{\circ} \mathrm{C} \\ 60-120 \text { seconds } \end{gathered}$ |
| Average ramp-up rate ( $\mathrm{T}_{\text {smax }}$ to $\mathrm{T}_{\mathrm{P}}$ ) | $3^{\circ} \mathrm{C} /$ second max. | $3^{\circ} \mathrm{C} /$ second max. |
| Liquidous temperature ( $\mathrm{T}_{\mathrm{L}}$ ) Time at liquidous ( $\mathrm{t}_{\mathrm{L}}$ ) | $\begin{gathered} 183{ }^{\circ} \mathrm{C} \\ 60-150 \text { seconds } \end{gathered}$ | $\begin{gathered} 217^{\circ} \mathrm{C} \\ 60-150 \text { seconds } \end{gathered}$ |
| $\begin{array}{l}\text { Peak } \\ \left(T_{p}\right)^{*}\end{array}$ | See Classification Temp in table 1 | See Classification Temp in table 2 |
| Time ( $\left.\mathrm{t}_{\mathrm{p}}\right)^{* *}$ within $5^{\circ} \mathrm{C}$ of the specified classification temperature ( $T_{c}$ ) | 20** seconds | 30** seconds |
| Average ramp-down rate ( $\mathrm{T}_{\mathrm{p}}$ to $\mathrm{T}_{\text {smax }}$ ) | $6^{\circ} \mathrm{C} /$ second max. | $6^{\circ} \mathrm{C} /$ second max. |
| Time $25^{\circ} \mathrm{C}$ to peak temperature | 6 minutes max. | 8 minutes max. |
| * Tolerance for peak profile Temperature ( $T_{p}$ ) is defined as a supplier minimum and a user maximum. <br> ** Tolerance for time at peak profile temperature ( $\mathrm{t}_{\mathrm{p}}$ ) is defined as a supplier minimum and a user maximum. |  |  |

Table 1. SnPb Eutectic Process - Classification Temperatures (Tc)

| Package <br> Thickness | ${\text { Volume } \mathbf{~ m m}^{3}}^{<350}$ | Volume mm $^{3}$ <br> $\geq 350$ |
| :---: | :---: | :---: |
| $<2.5 \mathrm{~mm}$ | $235^{\circ} \mathrm{C}$ | $220^{\circ} \mathrm{C}$ |
| $\geq 2.5 \mathrm{~mm}$ | $220^{\circ} \mathrm{C}$ | $220^{\circ} \mathrm{C}$ |

Table 2. Pb-free Process - Classification Temperatures (Tc)

| Package Thickness | $\begin{gathered} \text { Volume } \mathrm{mm}^{3} \\ <350 \end{gathered}$ | $\begin{aligned} & \text { Volume mm } \\ & 350-2000 \end{aligned}$ | $\begin{gathered} \text { Volume } \mathrm{mm}^{3} \\ >2000 \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| $<1.6$ mm | $260{ }^{\circ} \mathrm{C}$ | $260^{\circ} \mathrm{C}$ | $260^{\circ} \mathrm{C}$ |
| $1.6 \mathrm{~mm}-2.5 \mathrm{~mm}$ | $260^{\circ} \mathrm{C}$ | $250{ }^{\circ} \mathrm{C}$ | $245{ }^{\circ} \mathrm{C}$ |
| $\geq 2.5 \mathrm{~mm}$ | $250{ }^{\circ} \mathrm{C}$ | $245{ }^{\circ} \mathrm{C}$ | $245{ }^{\circ} \mathrm{C}$ |

## Reliability Test Program

| Test item | Method | Description |
| :--- | :--- | :--- |
| SOLDERABILITY | JESD-22, B102 | $5 \mathrm{Sec}, 245^{\circ} \mathrm{C}$ |
| HOLT | JESD-22, A108 | $1000 \mathrm{Hrs}, \mathrm{Bias} @ \mathrm{~T}_{\mathrm{j}}=125^{\circ} \mathrm{C}$ |
| PCT | JESD-22, A102 | $168 \mathrm{Hrs}, 100 \% \mathrm{RH}, 2 \mathrm{~atm}, 121^{\circ} \mathrm{C}$ |
| TCT | JESD-22, A104 | $500 \mathrm{Cycles},-65^{\circ} \mathrm{C} \sim 150^{\circ} \mathrm{C}$ |
| HBM | MIL-STD-883-3015.7 | VHBM 32 KV |
| MM | JESD-22, A115 | VMM $\geqq 200 \mathrm{~V}$ |
| Latch-Up | JESD 78 | $10 \mathrm{~ms}, 1 \mathrm{tr} \geq 100 \mathrm{~mA}$ |

## Customer Service

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